

# Vector Reconstruction – a new Gradient Computation Method

ECS Simulation Conference 2021

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# Quickstart

# The Key Information in less than 2 Minutes

Completely  
new method for stress  
gradient calculation:  
“Vector Reconstruction“

Only consideration of  
positive stress gradients  
(no support effect for  
stress increase)

Affects all modules  
with gradient  
(BASIC, MAX,  
SPECTRAL)

new handling of  
middle nodes in  
case of parabolic  
elements

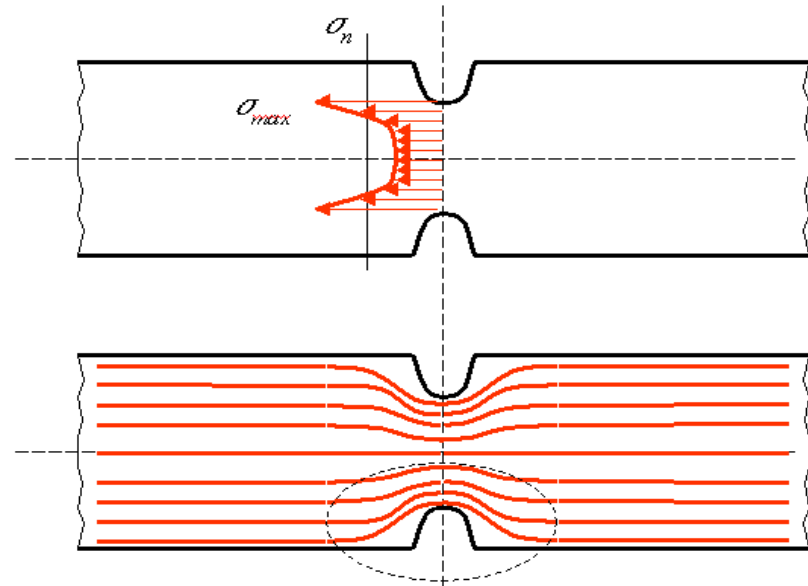
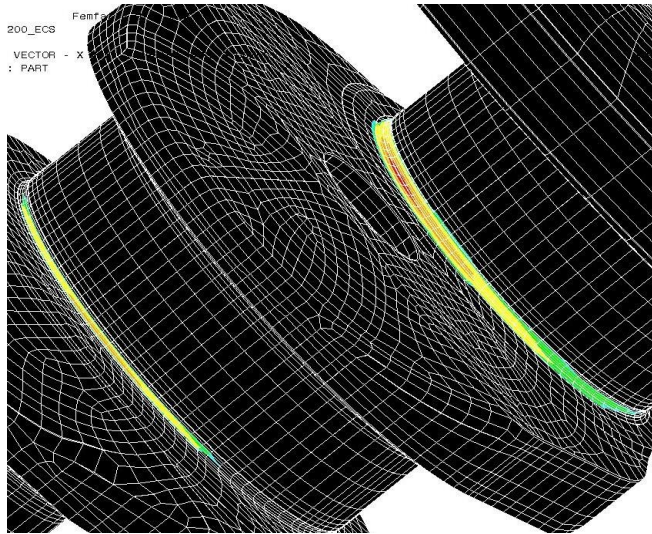


**Advantages:** max. gradient is computed (perpendicular to surface), unified method for all modules, no influence of number of channels in ChannelMAX.

# Introduction

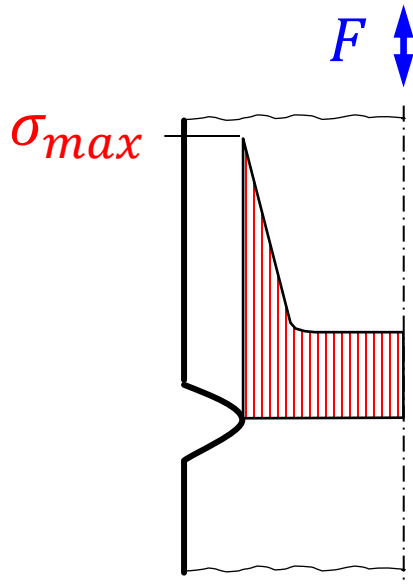
## What is the stress gradient?

Due to geometric and design properties, locations with stress concentrations (notches) often occur in reality. Typically the stress distribution is not constant, but has a peak in the notch with decaying values for the surrounding material.





How can we consider the stress gradient, how can it be computed for arbitrarily complex geometries?



The gradient is calculated from the difference of the stress tensors of neighboring nodes as well as their distance.

For fatigue analysis the relative stress gradient is used which is independent of the loading level

Stress Gradient

$$\chi = \frac{d\sigma}{dx}$$

Relative Stress Gradient

$$\chi' = \frac{1}{\sigma_{\max}} \left( \frac{d\sigma}{dx} \right)$$

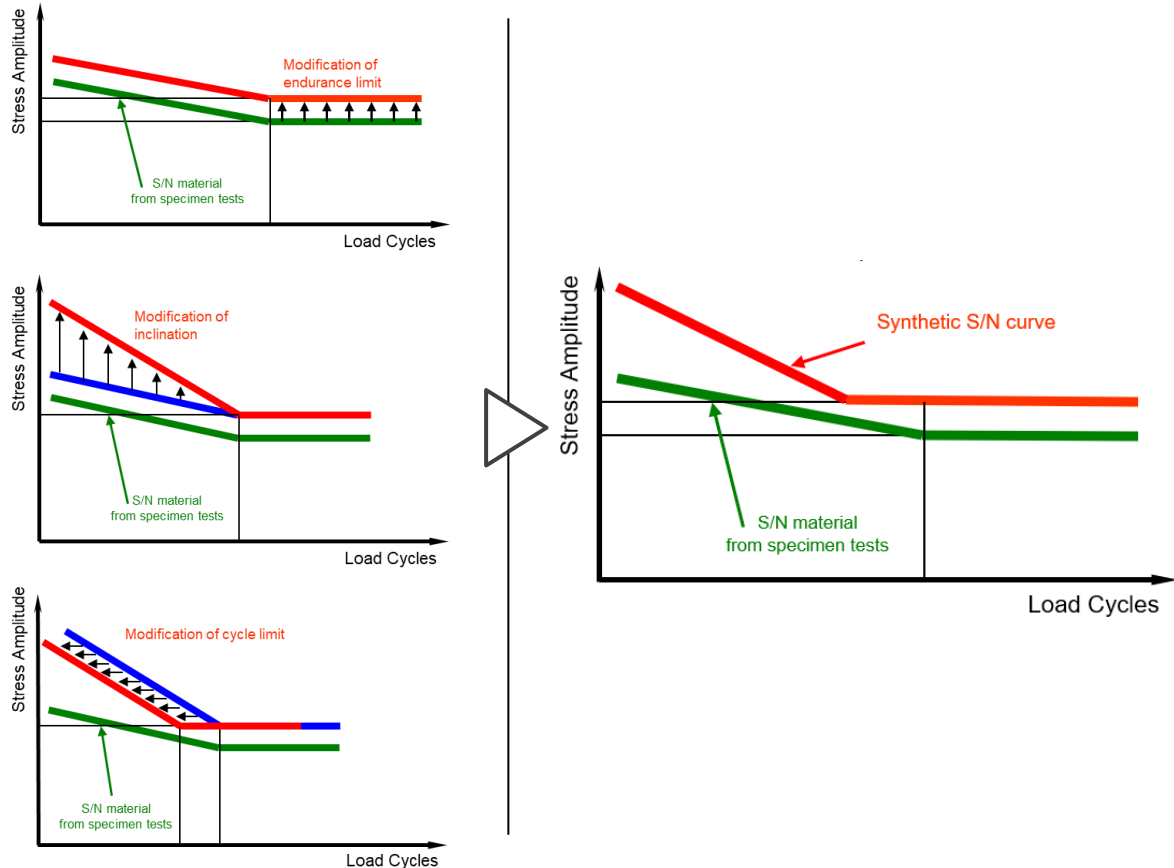
# Introduction in Four Questions (3/4)

## Why is the gradient such an important influence factor?

The locations of stress concentrations are critical to fatigue life.

The gradient has an influence on the component S/N curve and therefore on all fatigue results.

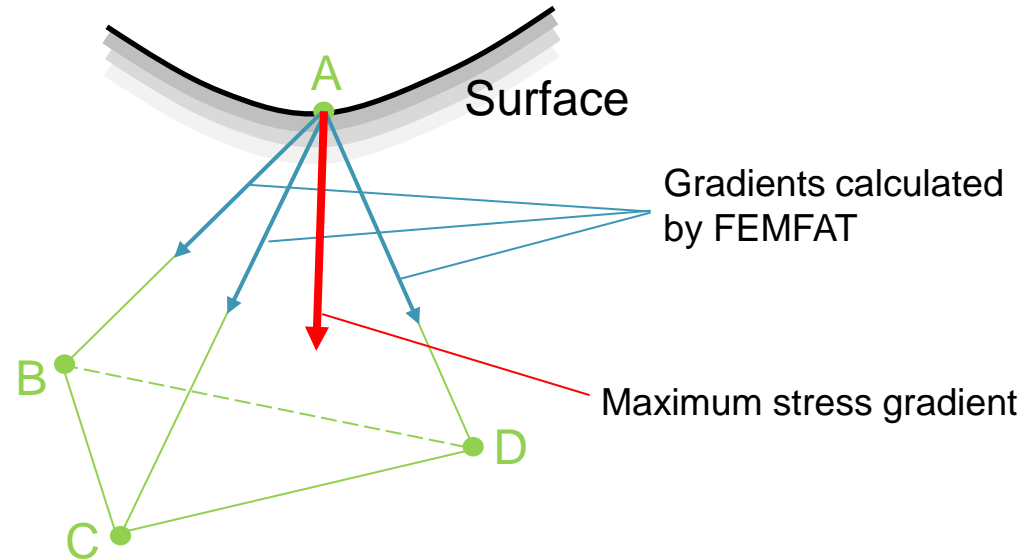
Therefore, you want to compute the stress gradient as accurate as possible.





## Why is there a new method, what does it make better than the default gradient?

- A complex shaped structure is usually meshed automatically with parabolic tetrahedrons
- FEMFAT calculates the stress gradient along Finite Element edges
- The maximum stress gradient is usually perpendicular to the surface
- But often there are no Finite Element edges perpendicular to the surface  
→ inaccurate results!



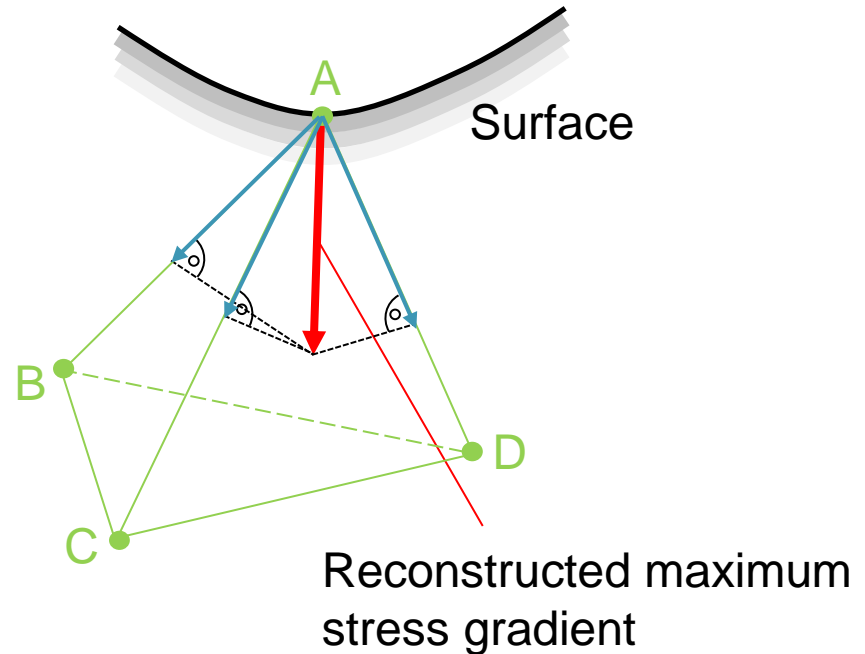
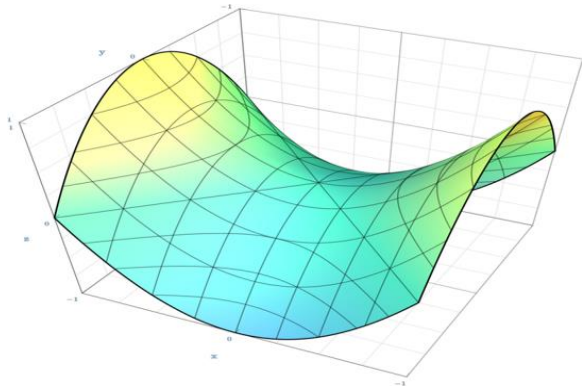
# New Gradient Method

# The new Gradient Method explained

A stress gradient is a vector pointing in the direction of the largest stress decrease.

It can be reconstructed by its components along the Finite Element edges.

$$\vec{\chi} = -\vec{\nabla}\sigma_{Mises} = -\begin{pmatrix} \frac{\partial\sigma_{Mises}}{\partial x} \\ \frac{\partial\sigma_{Mises}}{\partial y} \\ \frac{\partial\sigma_{Mises}}{\partial z} \end{pmatrix}$$



# New Stress Gradient Analysis Method



FEMFAT 5.4.2 - femfat

File View Analysis Options Templates Help

Current Working Directory: C:/FEMFATWORKDIR

**BASIC** | **Influence Factors**

- FE Entities
- Groups
- Stress Data
- Material Data
- Load Spectra
- Node Characteristics
- Influence Factors**

General Factors | Surface Treatment | WELD | SPOT

Stress Gradient

Gradient Computation Method: FEMFAT 2.4

Endurance Limit    Slope / Cycle Limit

Mean Stress

Endurance Limit    Slope / Cycle Limit

FEMFAT 2.4  
FEMFAT 2.4  
Vector Reconstruction

FEMFAT 4.1

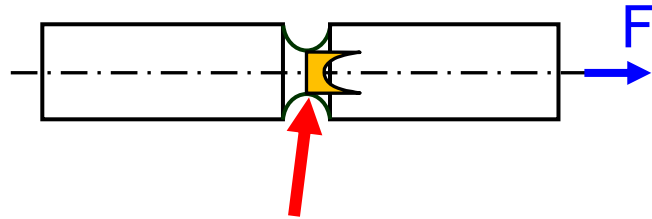
FEMFAT 5.1



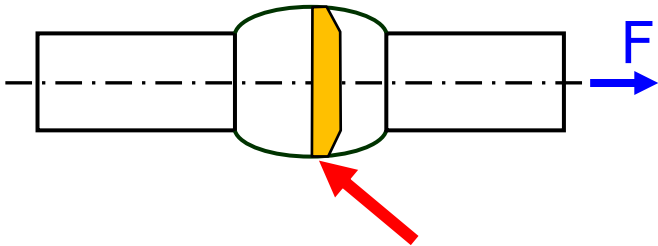
The new option “Vector Reconstruction” can be activated from the “Influence Factors” menu. “FEMFAT 2.4” method is still the default setting.

# New Stress Gradient Analysis Method

Only Finite Element edges with decreasing stresses are considered for gradient reconstruction, because there is no support effect for bulges („negative“ notches).



Decreasing stress → gradient influence

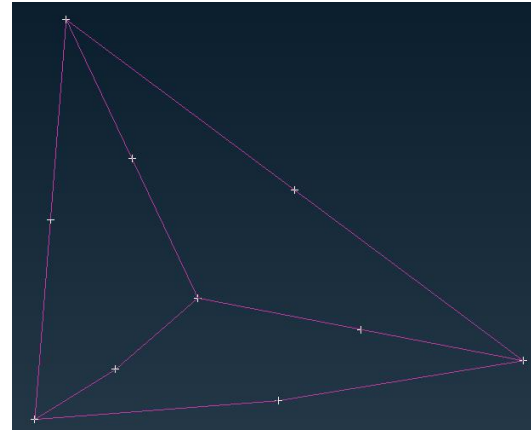
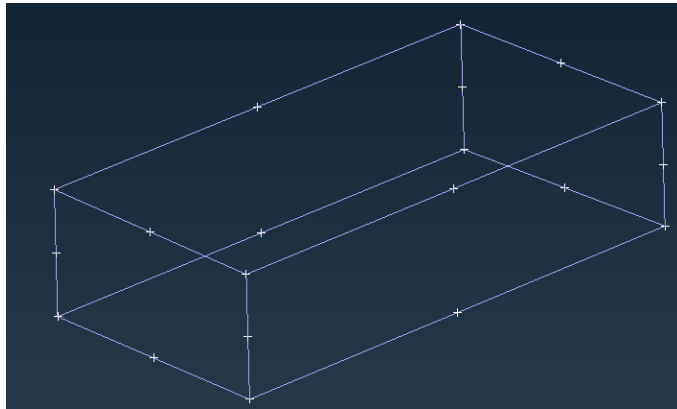


Increasing stress → NO gradient influence



# Different Handling for Middle Nodes of parabolic Elements

With activated “Vector Reconstruction” the gradients at middle nodes of parabolic elements are calculated directly, i.e. like corner nodes.

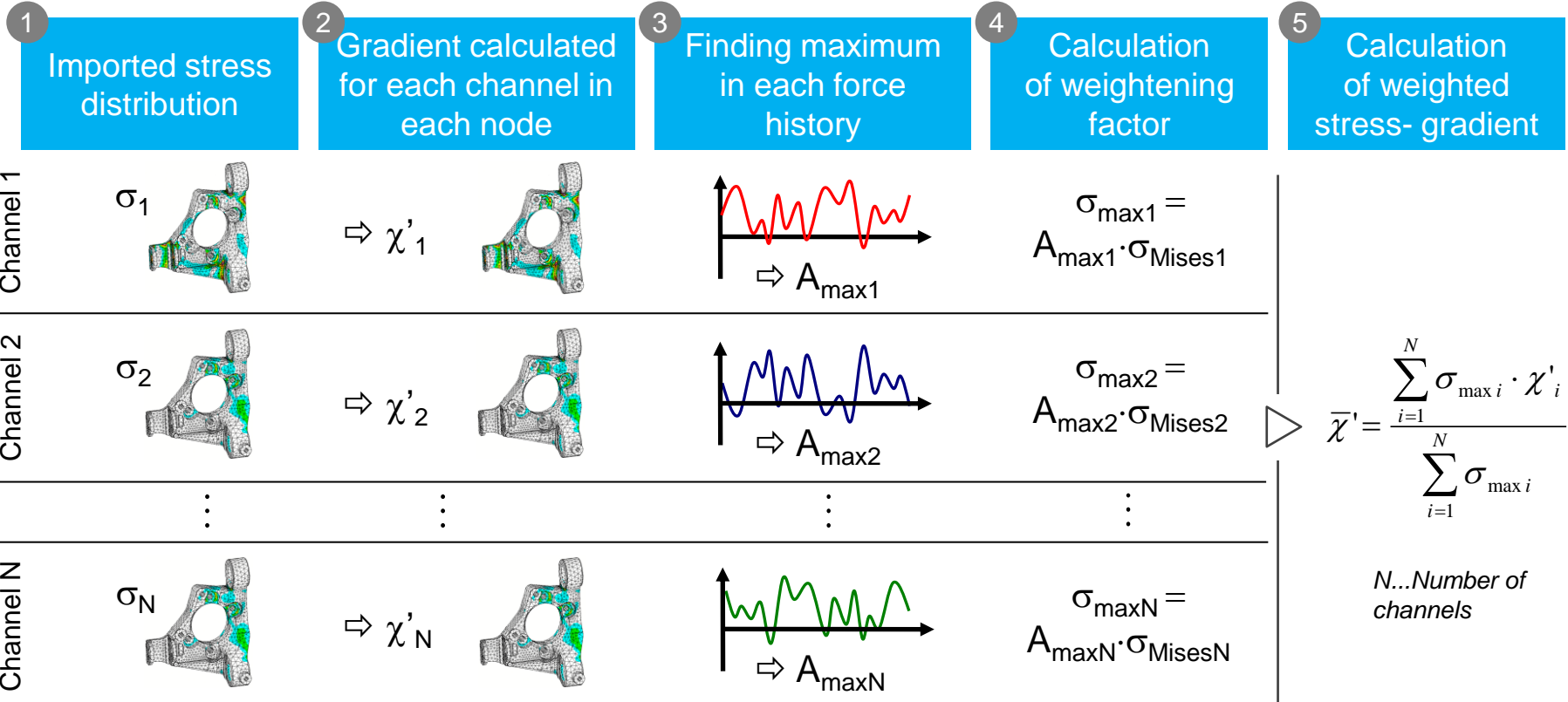


For the default setting “FEMFAT 2.4” the gradients at middle nodes are computed from the averaged gradients of the adjacent corner nodes.

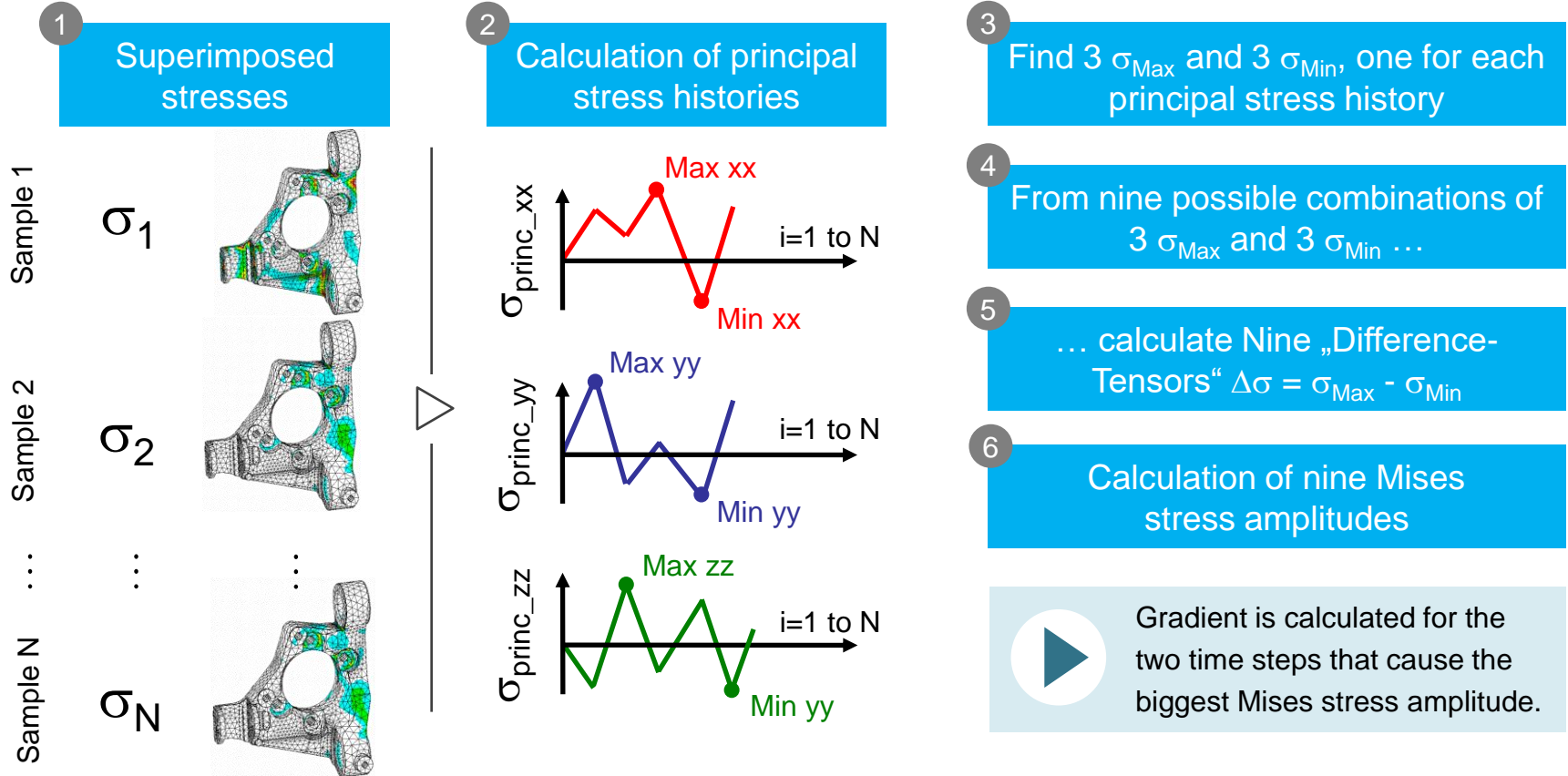
# Special Aspects in ChannelMAX



# ChannelMAX Gradient Analysis Old Method (“FEMFAT 2.4”)



# ChannelMAX Gradient Analysis **New Method** (“**Vector Reconstruction**“)

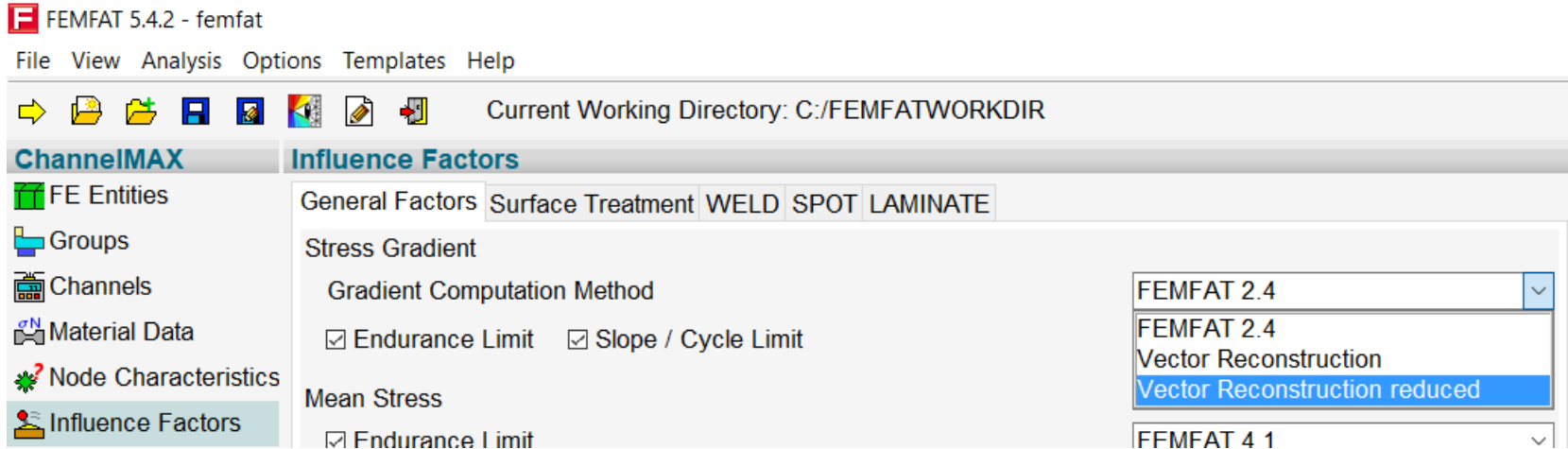


# Consequences of the “Vector Reconstruction” in ChannelMAX



- Usage of superimposed stresses **before** gradient computation & cutting plane analysis ensures the invariance of the Stress Gradient with respect to the analysis type (inertia relief or statically determined boundary conditions)
- Equivalent method to TransMAX and therefore identical results for identical loading.
- “Vector Reconstruction reduced” for an accelerated analysis with less time steps considered for superposition, but mostly same accuracy.

# “Vector Reconstruction reduced“ for accelerated Gradient Computation



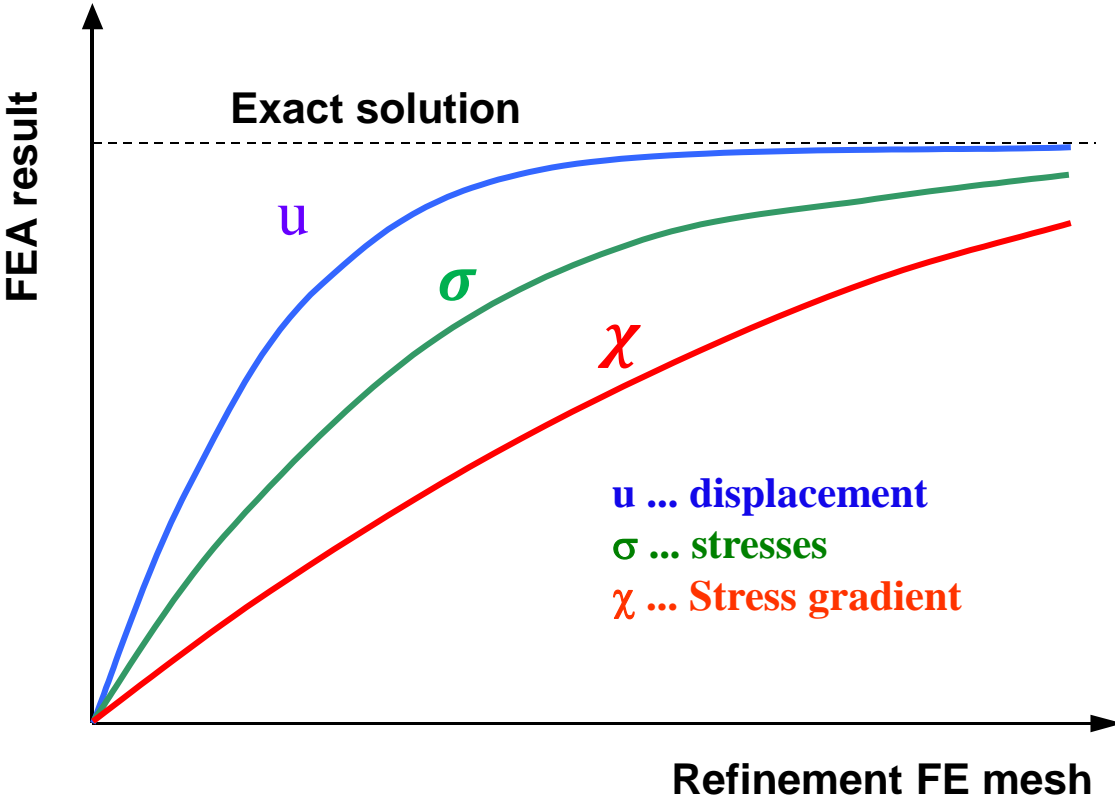
The screenshot shows the FEMFAT 5.4.2 software interface. The title bar reads "FEMFAT 5.4.2 - femfat". The menu bar includes "File", "View", "Analysis", "Options", "Templates", and "Help". The current working directory is "C:/FEMFATWORKDIR". The "ChannelMAX" sidebar is visible on the left, with "Influence Factors" selected. The "Influence Factors" dialog box is open, showing tabs for "General Factors", "Surface Treatment", "WELD", "SPOT", and "LAMINATE". Under "General Factors", the "Stress Gradient" section is active, showing "Gradient Computation Method" set to "FEMFAT 2.4". A dropdown menu is open, showing options: "FEMFAT 2.4", "Vector Reconstruction", "Vector Reconstruction reduced" (highlighted), and "FFMFAT 4 1". Other options include "Endurance Limit" and "Slope / Cycle Limit" (both checked), and "Mean Stress" with "Endurance Limit" checked.



The “Vector Reconstruction reduced” method takes only the maximum and minimum points in time of the load history records into account (i.e. a maximum of 2x number of channels).

# Comparison of Methods

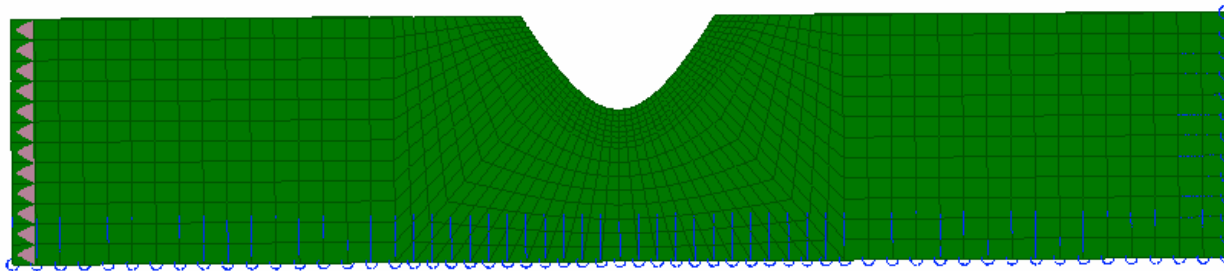
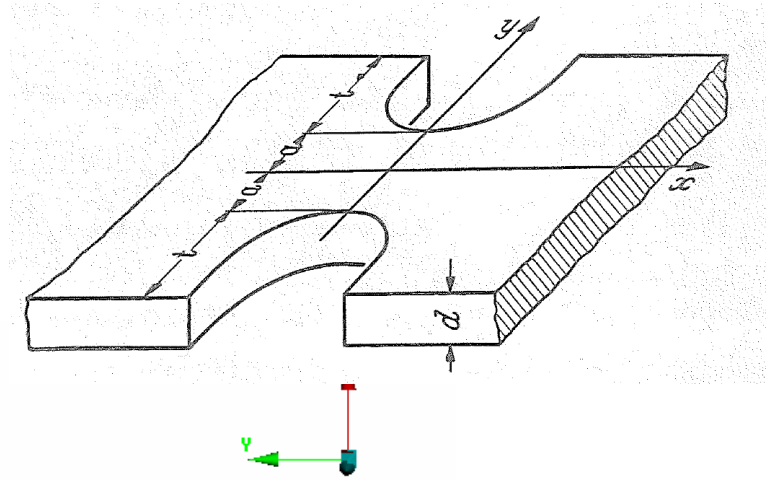
# Correlation between Accuracy and Type of Result



**As a derived quantity (from displacements), stress is always less precise!**

# First Example: Hyperbolic Notch

We consider a specimen with hyperbolic notch under tensile loading for which analytical expressions for the stresses\* are available. The focus is on the comparison of the different gradient methods in FEMFAT for several discretization levels.



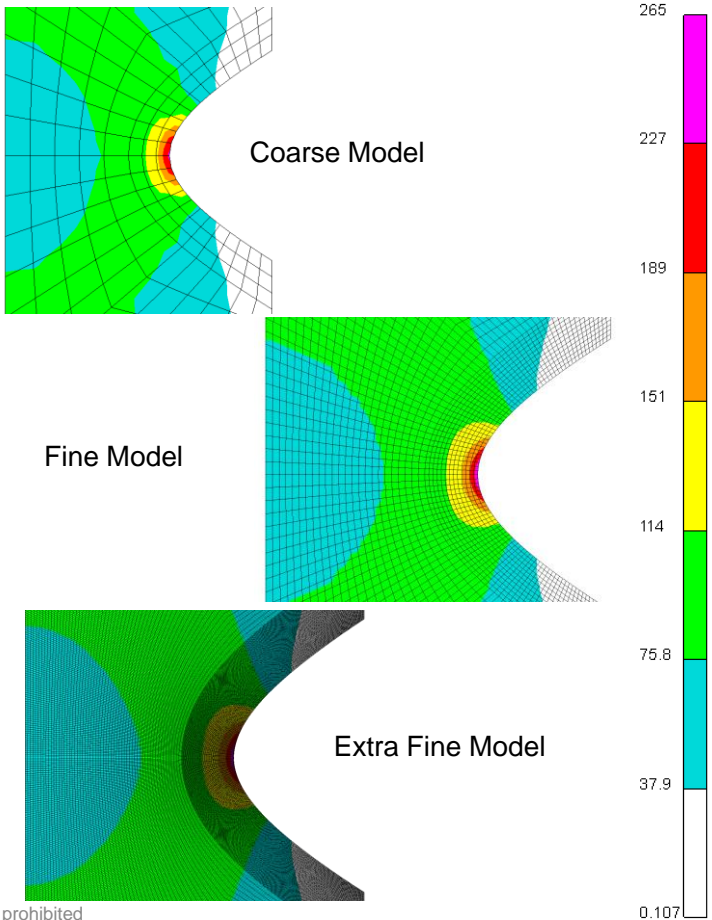
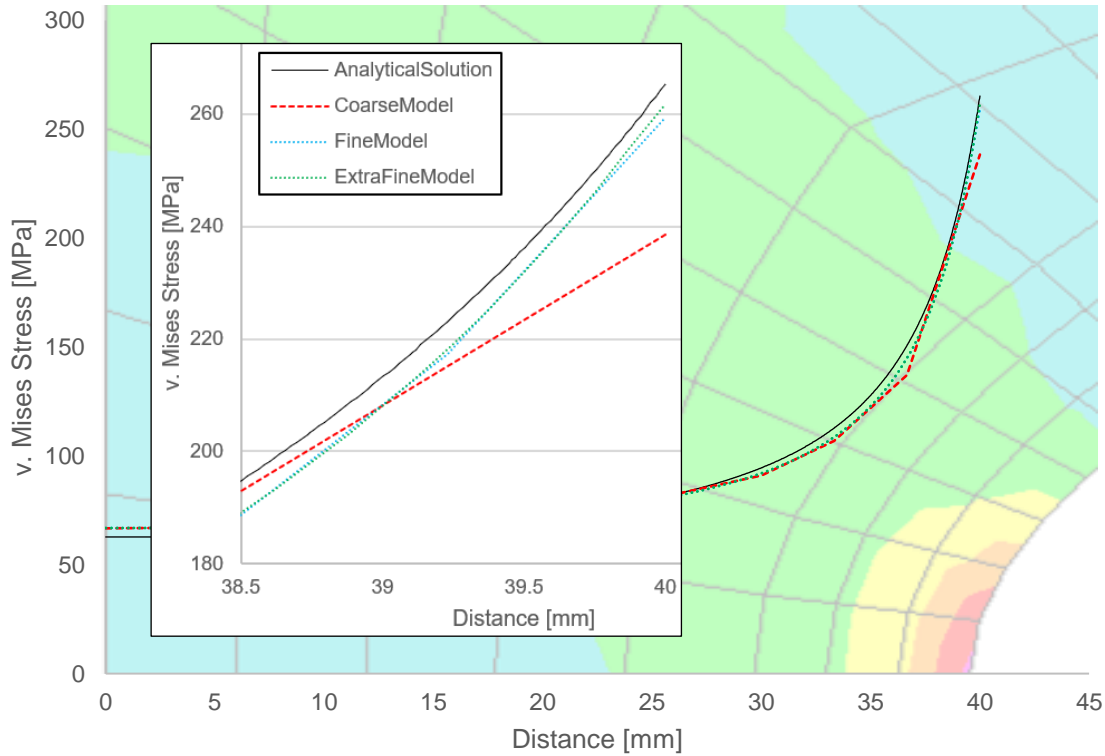
\*Neuber H.: Kerbspannungslehre, 2. Auflage, Springer Verlag, Berlin / Göttingen / Heidelberg, 1958



# Convergence Study



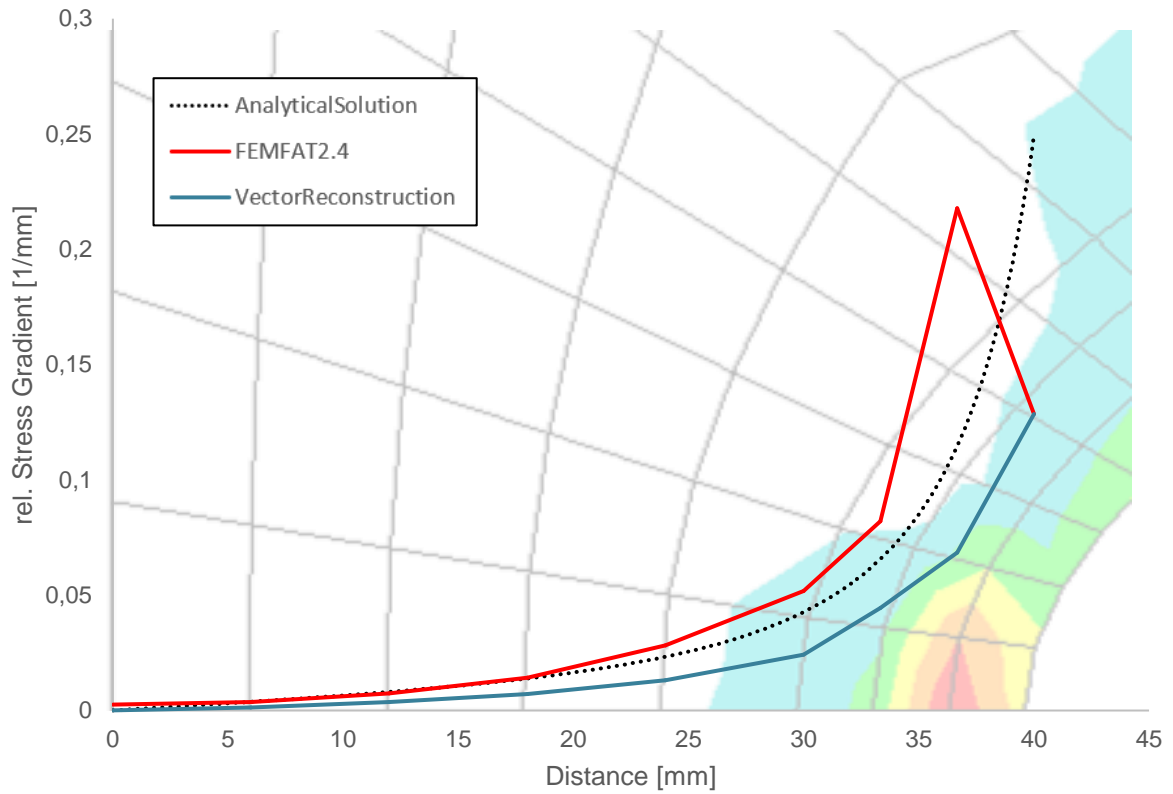
v. Mises Stresses [Mpa]



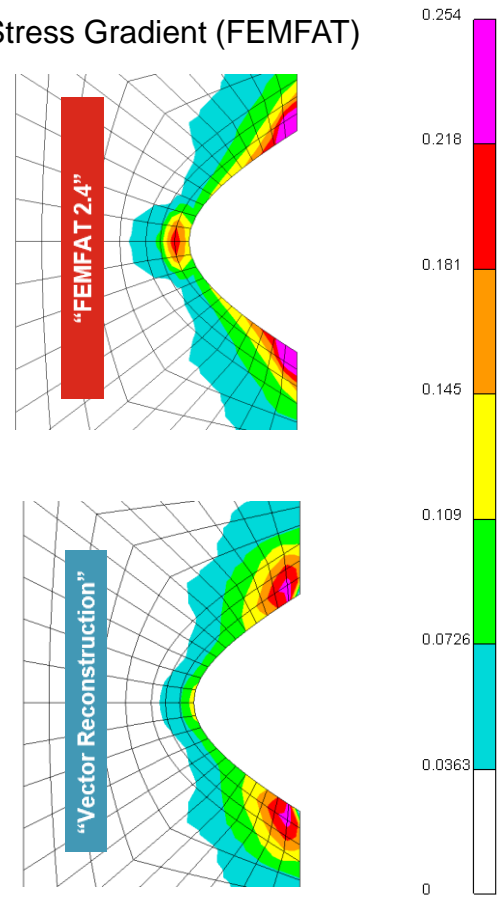
# Gradient Comparison for Coarse Model



### Rel. Stress Gradient (Hyperbola Notch Coarse Model)

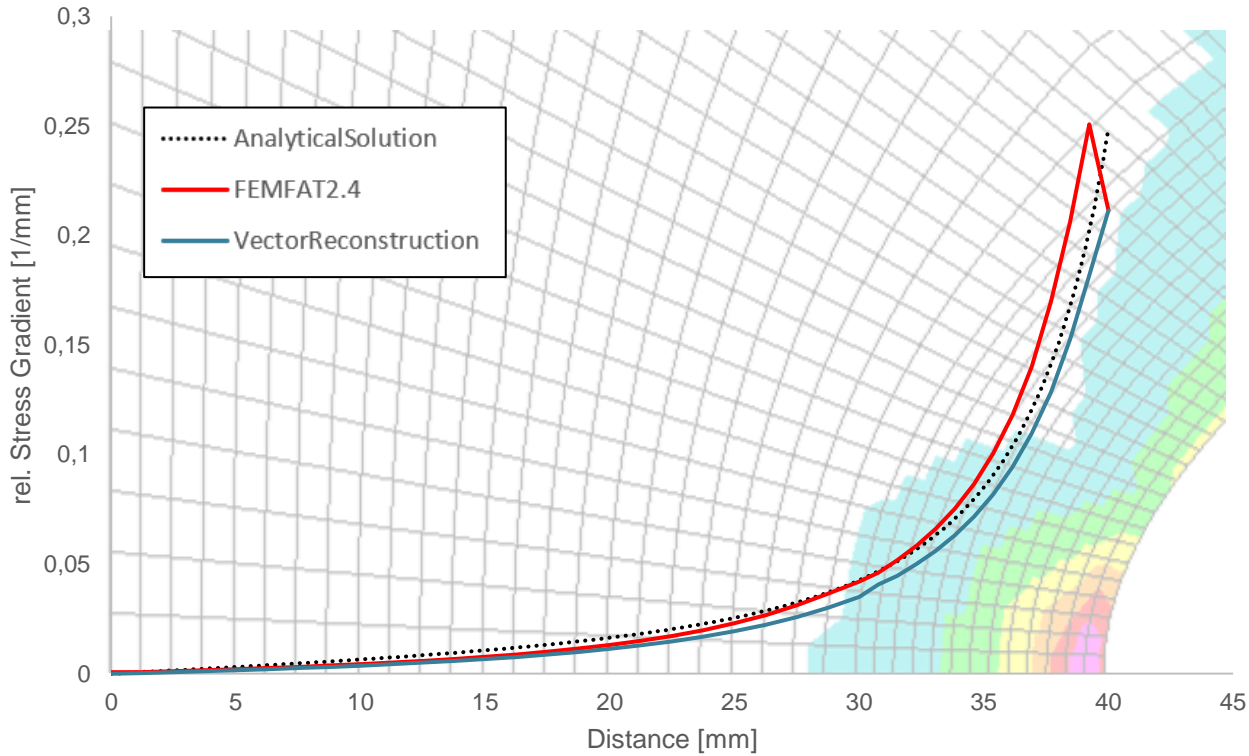


### Rel. Stress Gradient (FEMFAT)

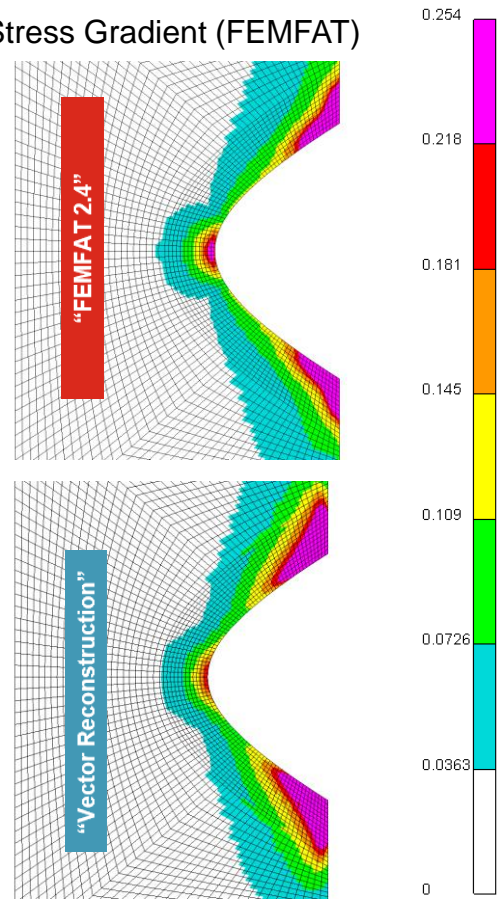


# Comparison for Fine Model

### Rel. Stress Gradient (Hyperbola Notch Fine Model)



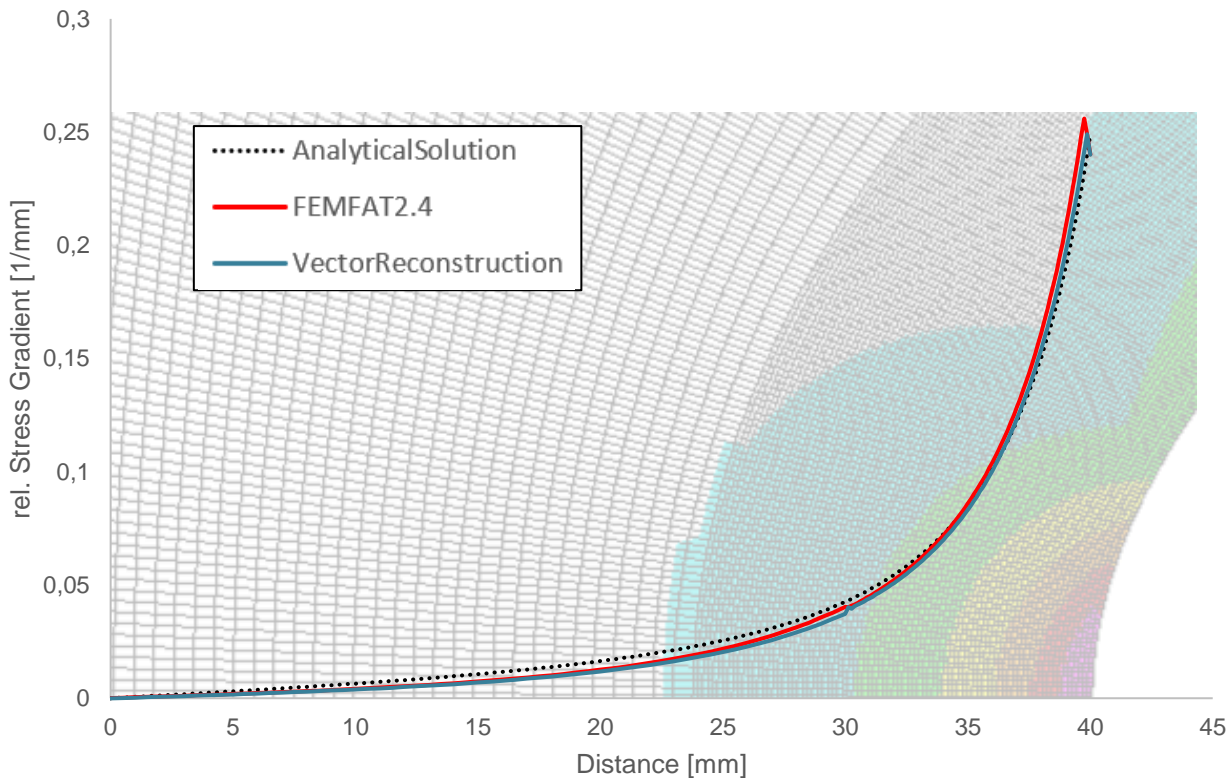
### Rel. Stress Gradient (FEMFAT)



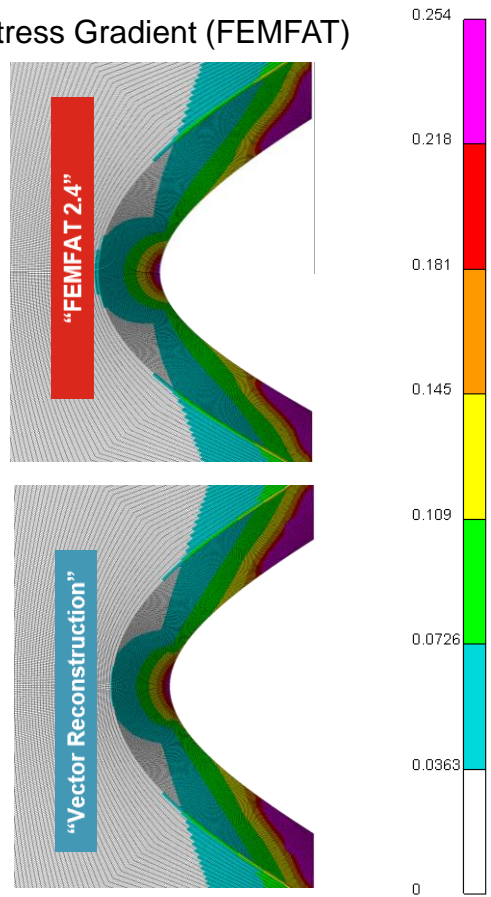
# Comparison for Extra Fine Model



Rel. Stress Gradient (Hyperbola Notch Extra Fine Model)



Rel. Stress Gradient (FEMFAT)



# Case Study



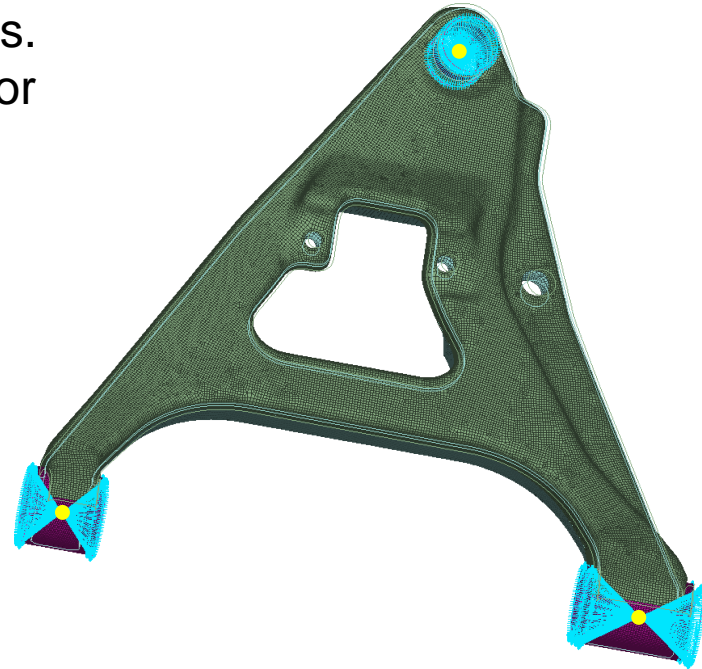
# Control Arm Case Study

## Task:

We consider a control arm modeled from shell elements. In FEA we analyse a total of 18 unit load cases (i.e. 6 for each interface node).

The subsequent fatigue analyses are carried out in ChannelMAX using random load histories for each channel.

The focus is on the comparison of damage results for different gradient methods (default “FEMFAT 2.4” and “Vector Reconstruction” resp.)



Number of Elements	~84000
Number of Nodes	~86000

Since in ChannelMAX the gradient is now calculated based on the superposed stress tensors, we also want to investigate the influence of the simulation method.

For this purpose, we use two different approaches in finite element analysis: Inertia Relief and Statically Determined Boundary Conditions.

Therefore we get four different fatigue analyses in ChannelMAX:

	“FEMFAT 2.4”	“Vector Reconstruction”
Stat. Determined	Analysis 1	Analysis 2
Inertia Relief	Analysis 3	Analysis 4



## “FEMFAT 2.4”

**Influence Factors**

General Factors | Surface Treatment | WELD | SPOT | LAMINATE

**Stress Gradient**

Gradient Computation Method: FEMFAT 2.4

Endurance Limit     Slope / Cycle Limit    FEMFAT 2.4

**Mean Stress**

Endurance Limit    FEMFAT 4.1

Slope / Cycle Limit    FEMFAT 5.1

Surface Roughness    FKM / IABG (Rz)

Mean (and Amplitude) Stress Rearrangement    **PLAST** Mean: Without Sequence Influence

Modified Haigh Diagram (Ultimate Tensile Strength)    Stress Gradient Influence

Technological Size Influence    FKM-Guideline

Statistical Influence    Gauss (LogN)

Isothermal Temperature Influence    FEMFAT 4.6

Cast Microstructure

Effective Plastic Strain    Method of Variable Slopes

Tempering Influence (for Tempering Steel only)

Surface Residual Stresses

Boundary Layer

Fiber Orientation    Logarithmic interpolation

Local Material Properties

Rotating Principal Stresses Influence    FEMFAT 4.2

Combination Method Influence Factors: FEMFAT 5.1

## “Vector Reconstruction”

**Influence Factors**

General Factors | Surface Treatment | WELD | SPOT | LAMINATE

**Stress Gradient**

Gradient Computation Method: Vector Reconstruction

Endurance Limit     Slope / Cycle Limit    FEMFAT 2.4

**Mean Stress**

Endurance Limit    FEMFAT 4.1

Slope / Cycle Limit    FEMFAT 5.1

Surface Roughness    FKM / IABG (Rz)

Mean (and Amplitude) Stress Rearrangement    **PLAST** Mean: Without Sequence Influence

Modified Haigh Diagram (Ultimate Tensile Strength)    Stress Gradient Influence

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Local Material Properties

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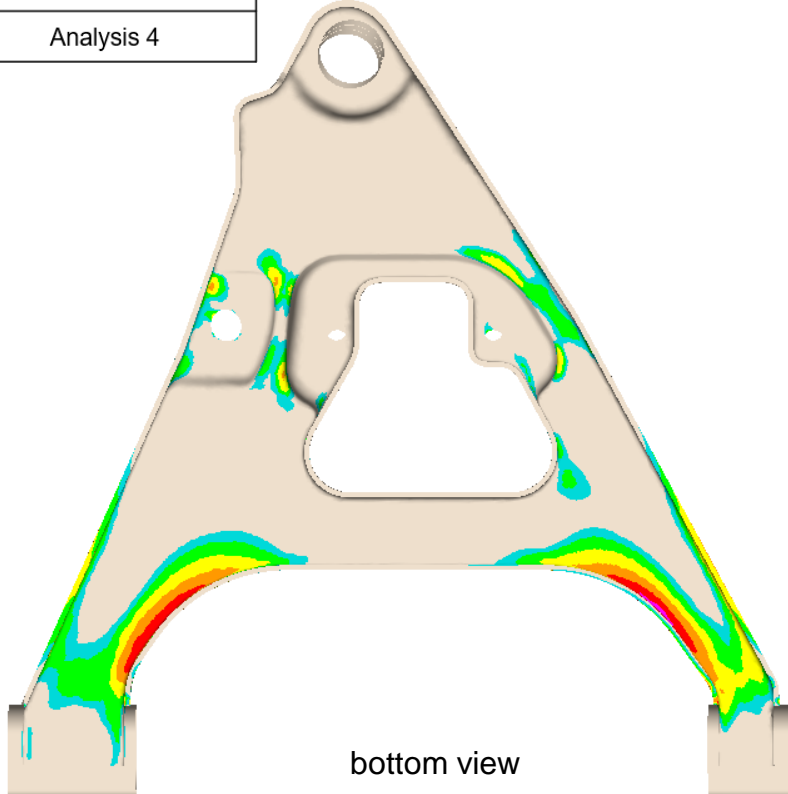
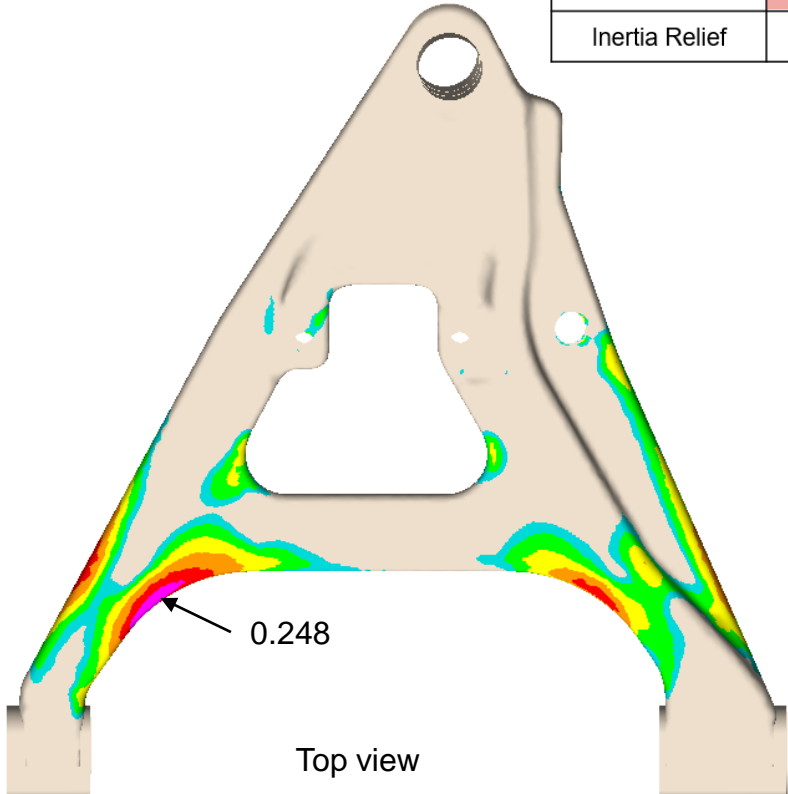
Combination Method Influence Factors: FEMFAT 5.1

# Results Comparison for Different Gradient Methods

# Damage Results



	“FEMFAT 2.4”	“Vector Reconstruction”
Stat. Determined	Analysis 1	Analysis 2
Inertia Relief	Analysis 3	Analysis 4

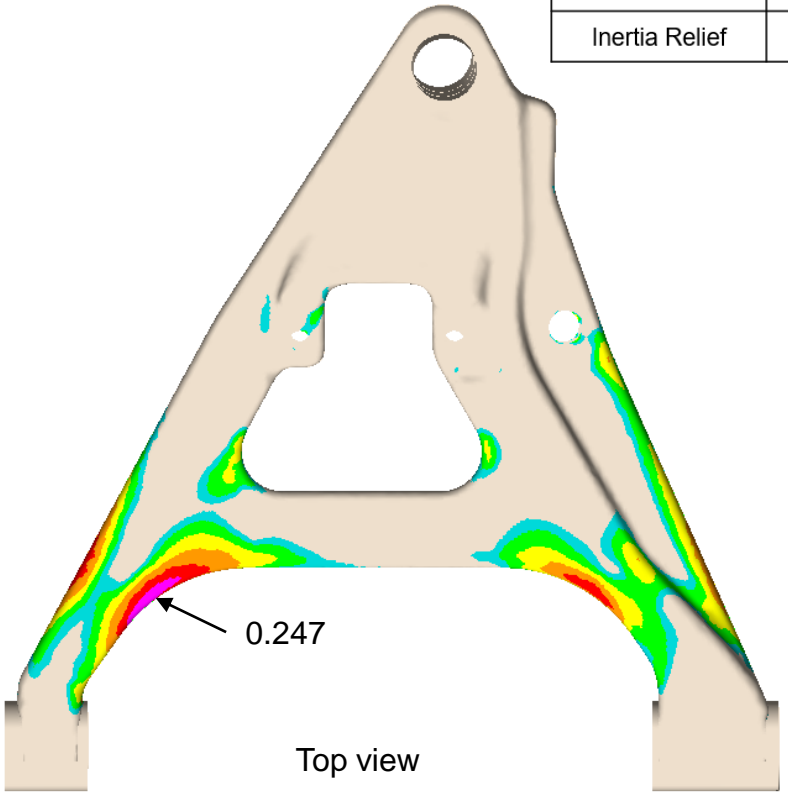


# Damage Results

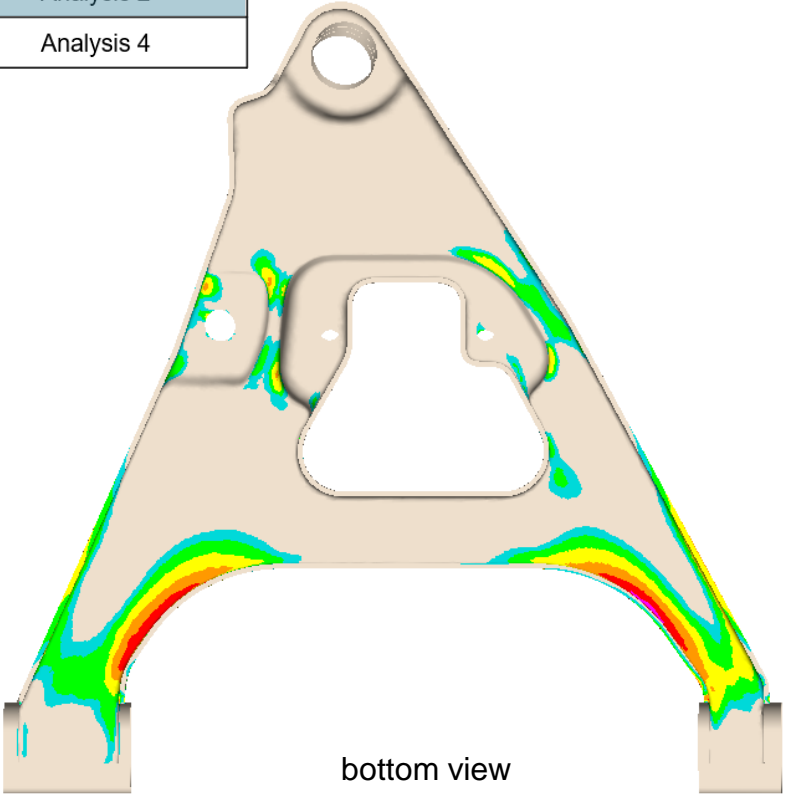
# “Vector Reconstruction”



	“FEMFAT 2.4”	“Vector Reconstruction”
Stat. Determined	Analysis 1	Analysis 2
Inertia Relief	Analysis 3	Analysis 4



Top view



bottom view

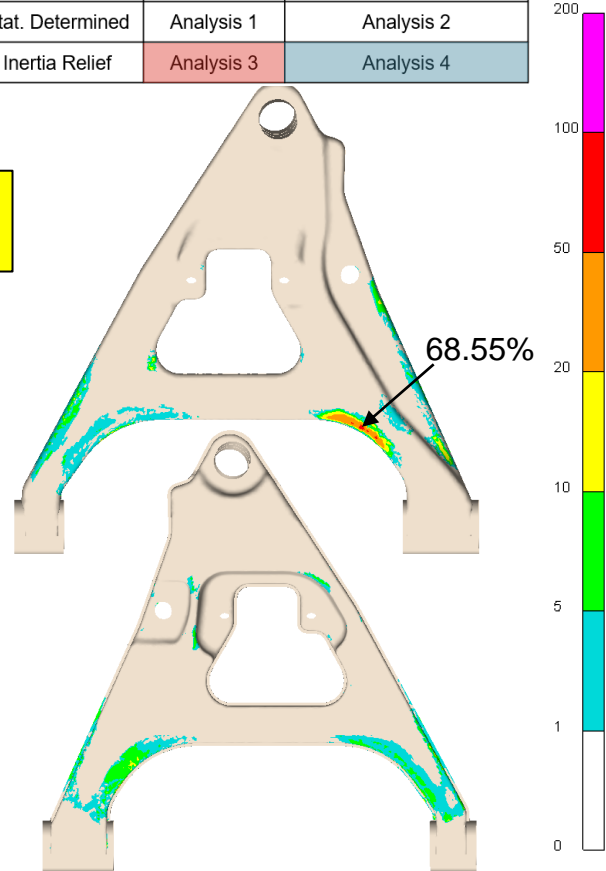
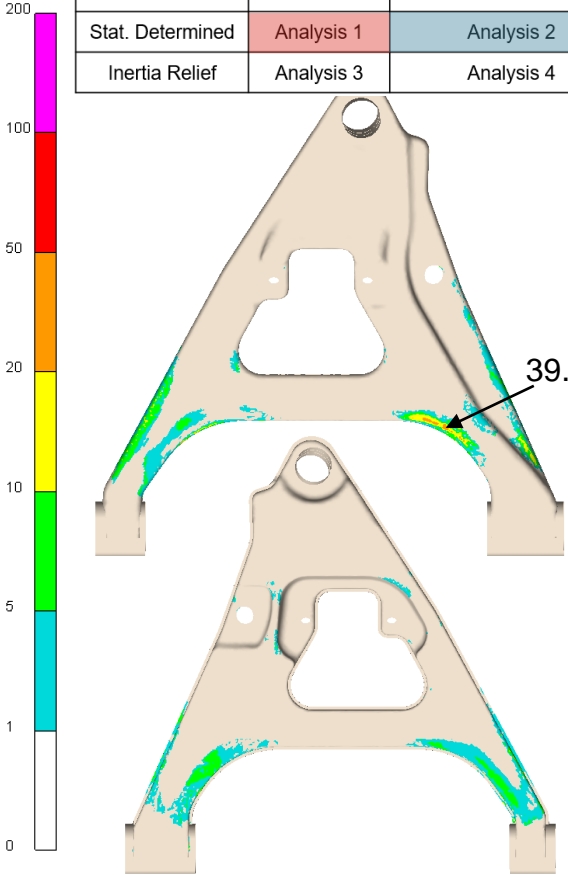
# Damage Discrepancy $\Delta_{\text{Damage}}$



	"FEMFAT 2.4"	"Vector Reconstruction"
Stat. Determined	Analysis 1	Analysis 2
Inertia Relief	Analysis 3	Analysis 4

	"FEMFAT 2.4"	"Vector Reconstruction"
Stat. Determined	Analysis 1	Analysis 2
Inertia Relief	Analysis 3	Analysis 4

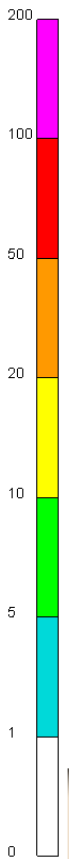
$$\Delta_{\text{Damage}} := 100 * \frac{|D_{\text{Femat24}} - D_{\text{VectorRec}}|}{D_{\text{Femat24}}}$$



# Results Comparison for FEA Simulation Methods

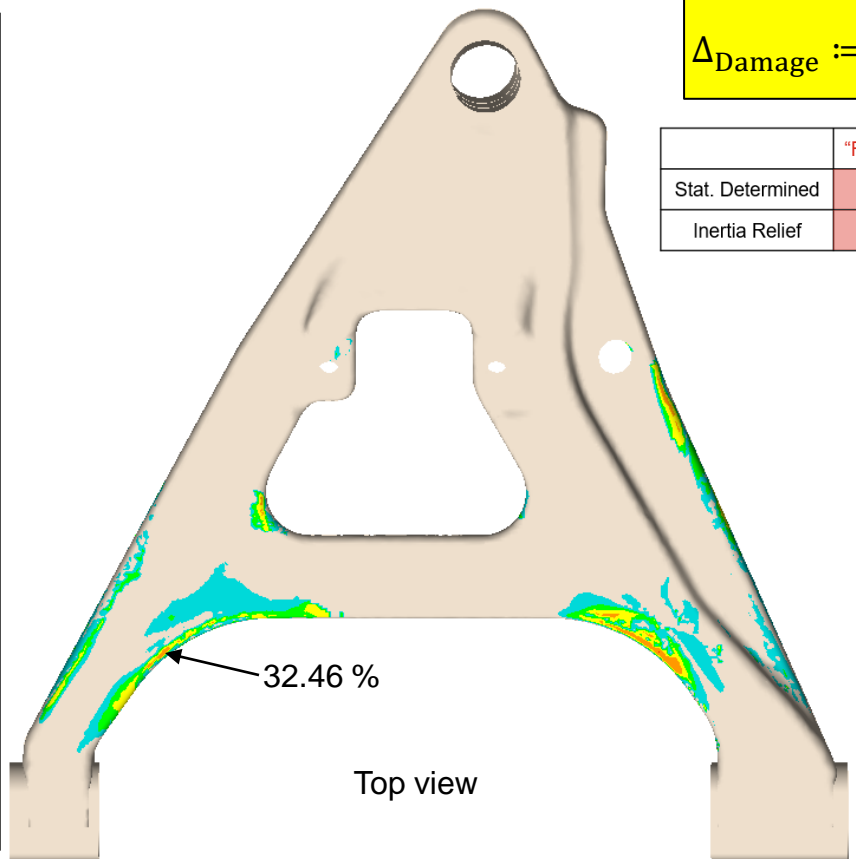
# Damage Discrepancy $\Delta_{\text{Damage}}$

**"FEMFAT 2.4"**

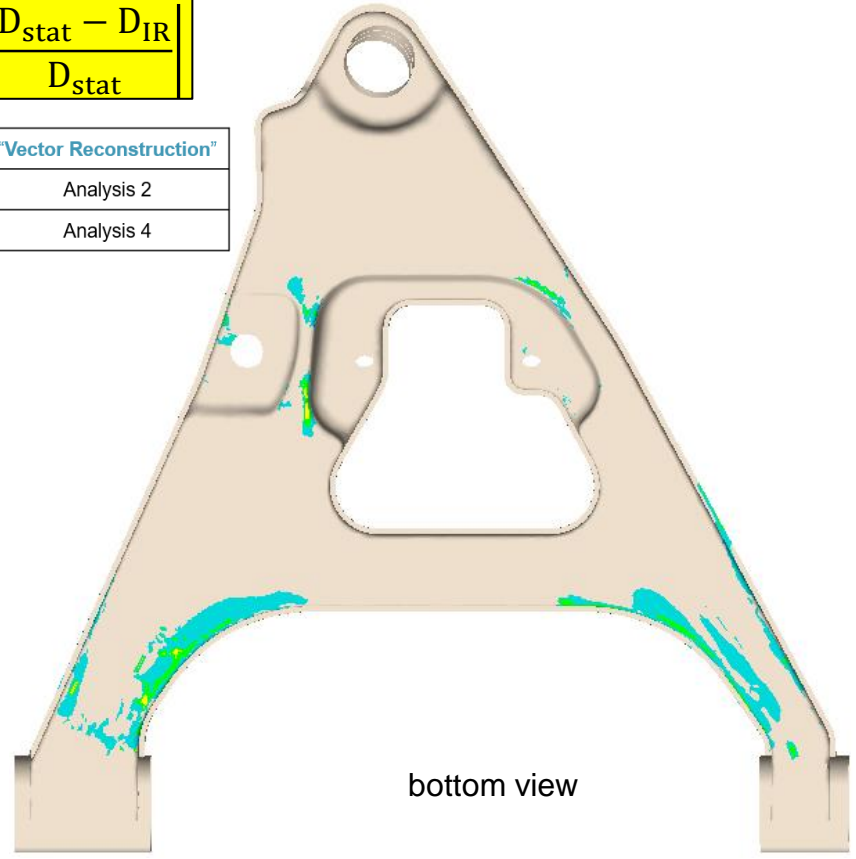


$$\Delta_{\text{Damage}} := 100 * \frac{|D_{\text{stat}} - D_{\text{IR}}|}{D_{\text{stat}}}$$

	"FEMFAT 2.4"	"Vector Reconstruction"
Stat. Determined	Analysis 1	Analysis 2
Inertia Relief	Analysis 3	Analysis 4



Top view

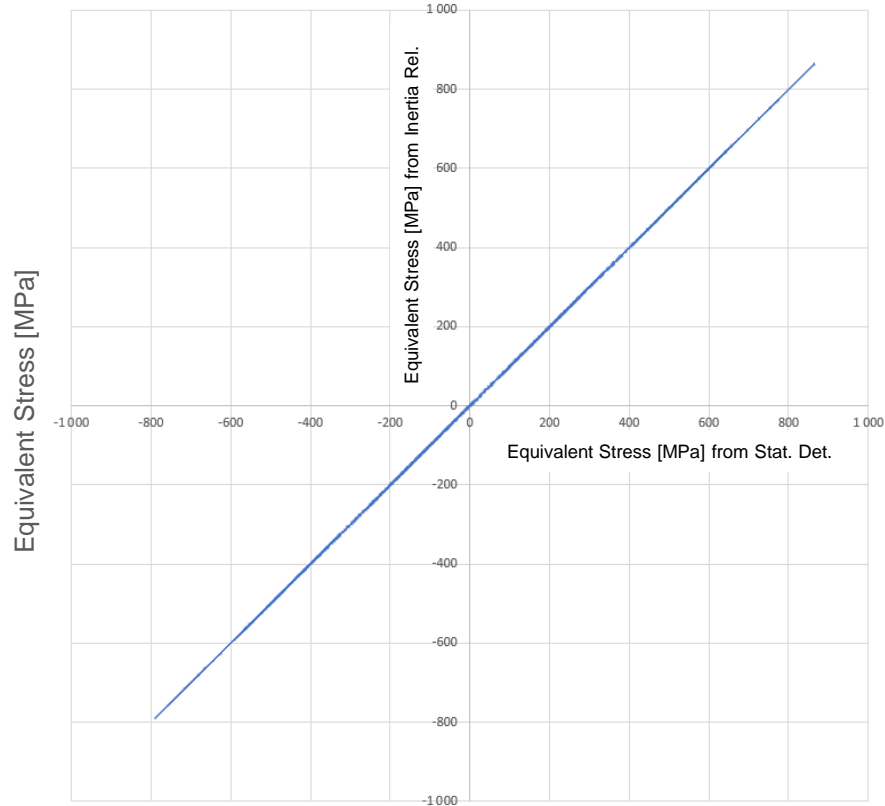


bottom view





## Local Equivalent Stress History

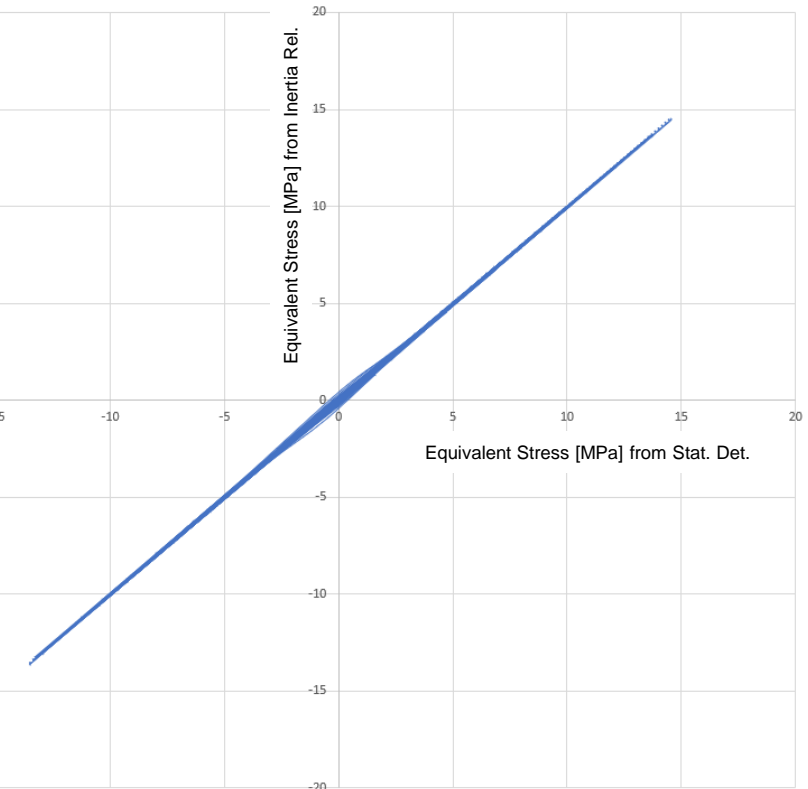


## Detailed Local Results

	Inertia Relief	Statically Determined	
<b>Damage [-]</b>	0.1672	0.248	✗
<b>Rel. Stress Gradient [1/mm]</b>	0.0677	0.048	✗
<b>Stress Ampl. [MPa]</b>	835.1	835.1	✓
<b>Mean Stress [MPa]</b>	5.32	5.32	✓
<b>Local Fatigue Limit [MPa]</b>	290.9	288.7	✗
<b>Local Slope [-]</b>	10.96	11.31	✗
<b>Local Cycle Limit [-]</b>	1.903E06	1.935E06	✗



## Local Equivalent Stress History

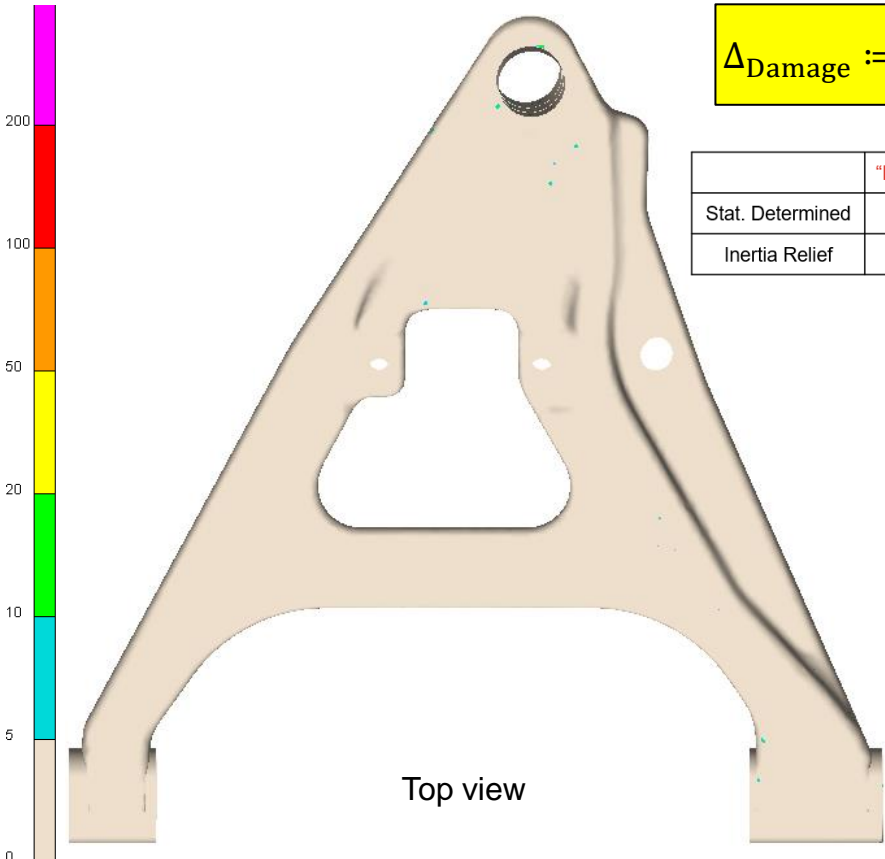


## Detailed Local Results

	Inertia Relief	Statically Determined	
<b>Damage [-]</b>	1.566E-13	5.074E-13	✗
<b>Rel. Stress Gradient [1/mm]</b>	2.616	5.455	✗
<b>Stress Ampl. [MPa]</b>	14.27	14.08	✓
<b>Mean Stress [MPa]</b>	0.46	0.46	✓
<b>Local Fatigue Limit [MPa]</b>	383.4	440.8	✗
<b>Local Slope [-]</b>	3.34	3.095	✗
<b>Local Cycle Limit [-]</b>	5.757E05	5.029E05	✗

# Damage Discrepancy $\Delta_{\text{Damage}}$

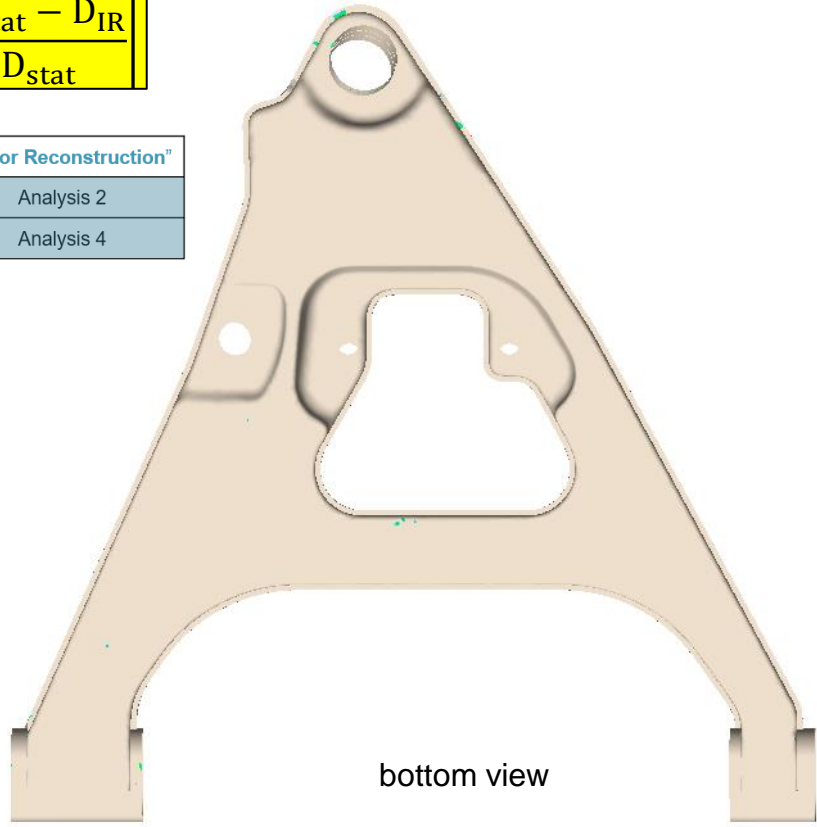
# “Vector Reconstruction”



Top view

$$\Delta_{\text{Damage}} := 100 * \frac{|D_{\text{stat}} - D_{\text{IR}}|}{D_{\text{stat}}}$$

	"FEMFAT 2.4"	"Vector Reconstruction"
Stat. Determined	Analysis 1	Analysis 2
Inertia Relief	Analysis 3	Analysis 4

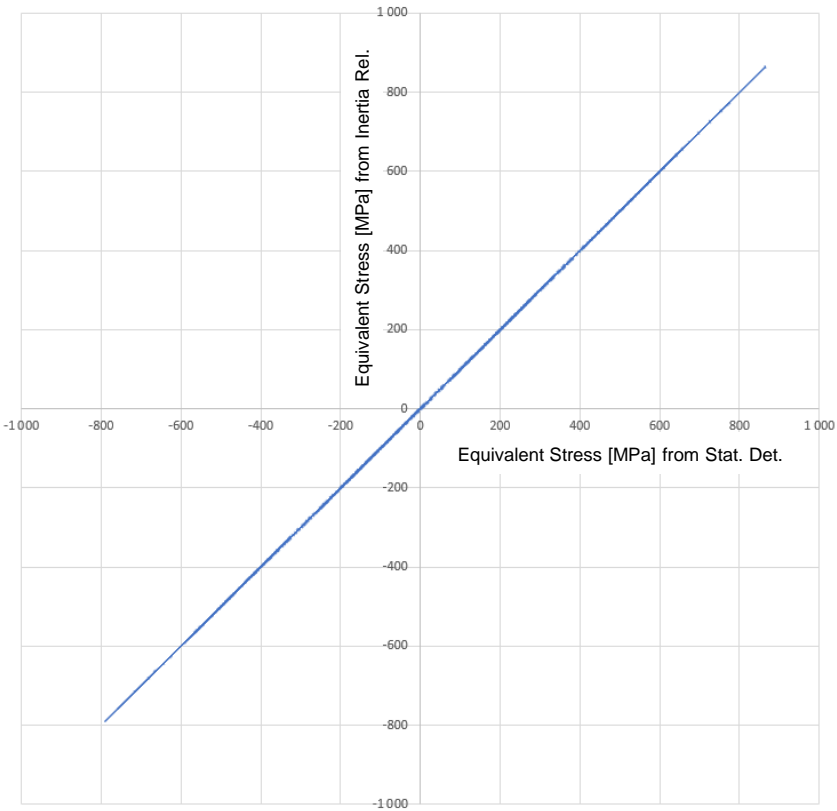


bottom view

# Results Node 1 (max. Damage) “Vector Reconstruction”



## Local Equivalent Stress History



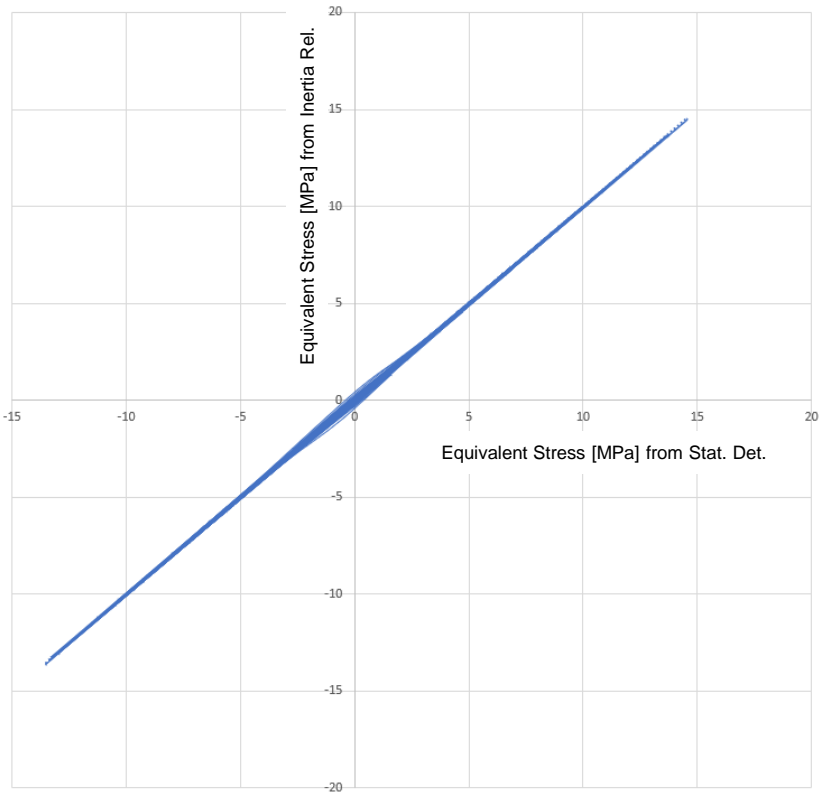
## Detailed Local Results

	Inertia Relief	Statically Determined	
<b>Damage [-]</b>	0.247	0.247	✓
<b>Rel. Stress Gradient [1/mm]</b>	0.047	0.047	✓
<b>Stress Ampl. [MPa]</b>	825.9	825.9	✓
<b>Mean Stress [MPa]</b>	9.62	9.62	✓
<b>Local Fatigue Limit [MPa]</b>	288.1	288.1	✓
<b>Local Slope [-]</b>	11.39	11.39	✓
<b>Local Cycle Limit [-]</b>	1.936E06	1.936E06	✓

# Results Node 2 (max. Gradient) “Vector Reconstruction”



## Local Equivalent Stress History



## Detailed Local Results

	Inertia Relief	Statically Determined	
<b>Damage [-]</b>	4.82E-13	4.83E-13	✓
<b>Rel. Stress Gradient [1/mm]</b>	7.51	7.51	✓
<b>Stress Ampl. [MPa]</b>	14.05	14.03	✓
<b>Mean Stress [MPa]</b>	0.67	0.72	✓
<b>Local Fatigue Limit [MPa]</b>	474.7	474.7	✓
<b>Local Slope [-]</b>	3.055	3.055	✓
<b>Local Cycle Limit [-]</b>	4.906E05	4.906E05	✓

# Performance of “Vector Reconstruction” Method

Control Arm example, single CPU run:

Analysis Duration	“Vector Reconstruction”	Method “FEMFAT 2.4”	“Vector Reconstr. Reduced”
Inertia Relief	650 sec	489 sec	477 sec
Statically Determined	561 sec	431 dec	429 sec



The ratio seen here also applies in general: the “Vector Reconstruction” method leads to approximately 30% longer analysis running time.

# Summary

- As of FEMFAT 5.4.2 a completely new method for relative stress gradient calculation (“Vector Reconstruction“) is available.
- The new method can be used in all modules with gradient computation (BASIC, MAX, SPECTRAL).
- Big advantage: identification of max. gradient, unified method for all modules, invariant for different simulation techniques (Inertia Relief or Statically Determined Boundary conditions).
- Two additional aspects for ChannelMAX:
  - Gradient is computed on basis of superimposed stress tensors (analoguous to TransMAX)
  - third method „Vector Reconstruction Reduced“ for improved performance





DRIVING **EXCELLENCE.**  
INSPIRING **INNOVATION.**